



**NORTHLAND
POWER**

Long Lake Solar Project Noise Assessment Study Report

August 8, 2013



Northland Power Inc.
on behalf of
Northland Power Solar
Long Lake L.P.
Toronto, Ontario

Noise Assessment Study Report

Long Lake Solar Project

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Executive Summary

This report presents the results of the Noise Assessment Study required for Solar Facilities under Ontario Regulation 359/09 and 521/10, as part of the Renewable Energy Approval (REA) Process. Northland Power Solar Long Lake L.P. (“Northland”) is proposing to develop a 10-megawatt (MW) solar photovoltaic (PV) project titled Long Lake Solar Project (the “Project”). The Project will be located on approximately 46 hectares (ha) of land within the unorganized township of Calder, District of Cochrane.

This Noise Assessment Study Report has been prepared based on the document entitled “Basic Comprehensive Certificates of Approval (Air) – User Guide” by the Ontario Ministry of the Environment (MOE, 2004). The sound pressure levels at the points of reception (POR) have been estimated using ISO 9613-2, implemented in the CADNA-A computer code. The performance limits used for verification of compliance correspond to the values for rural areas of 40 dBA. The results presented in this report are based on the best available information at this time. It is the intention that, in the detailed engineering phase of the project, certified noise data based on final plans and designs will confirm the conclusions of this noise impact assessment study.

The results obtained in this study show that the sound pressure levels at POR, resulting from the Project operation, will not exceed MOE requirements for rural areas of 40 dBA.

Project Report

August 8, 2013

**Northland Power Inc.
Long Lake Solar Project**

Noise Assessment Study Report

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1. Introduction

1.1 Project Description

Northland Power Solar Long Lake L.P. (“Northland”) is proposing to develop a 10-megawatt (MW) solar photovoltaic (PV) project titled Long Lake Solar Project (the “Project”). The Project will be located on approximately 46 ha of land within the unorganized township of Calder, District of Cochrane.

The proposed Project is a renewable energy generation facility which will use solar photovoltaic technology to generate electricity. Electricity generated by solar photovoltaic panels will be converted from Direct Current (DC) to Alternating Current (AC) by inverter clusters which will also step up the voltage to 27.6 kV. A main transformer, located in the substation, will step up the voltage from the clusters to 115 kV prior to being transmitted to the existing local distribution line. In order to meet the Ontario Power Authority (OPA)’s Feed-In-Tariff (FIT) Program requirements, a specific percentage of equipment will be manufactured in Ontario.

The construction of the Project will begin once the Renewable Energy Approval (REA) has been obtained and a power purchase agreement is finalized with the OPA. The anticipated operational lifespan of the Project is 30 years.

1.2 Renewable Energy Approval Legislative Requirements

Ontario Regulation 359/09 and 521/10, made under the Environmental Protection Act identify the Renewable Energy Approval (REA) requirements for green energy projects in Ontario. As per Section 4 of these regulations, ground mounted solar facilities with a name plate capacity greater than 12 kilowatts (kW) are classified as a Class 3 solar facility and, therefore, require an REA.

Section 13 of the Ontario Regulation 359/09 requires proponents of Class 3 solar facilities to complete a Noise Study Report in accordance with Appendix A of the publication; “Basic Comprehensive Certificates of Approval (Air) – User Guide, 2004” by the Ministry of the Environment (MOE, 2004).

The Noise Study Report is to include a general description of the facility, sources and points of reception (POR), Assessment of compliance, as well as all the supporting information relevant to the Project. A draft of the Noise Study Report must be made available to the public, the local municipality and identified Aboriginal communities, at least 60 days prior to the final public consultation meeting in accordance with Ontario Regulation 359/09 and 521/10.

2. Facility Description

The Project will utilize photovoltaic (PV) panels installed on fixed racking structures mounted on the ground. The PV panels generate DC electricity which will be converted to AC electricity by inverters. The Project layout is based on seven inverter clusters each one containing two inverters and one medium-voltage (360-V /27.6-kV/1.6-MVA) transformer, and one 27.6-kV/115-kV/10-MVA substation transformer. The 27.6-kV power, collected from the inverter clusters, will be stepped up to 115 kV by the substation transformer prior to being transmitted to the existing local distribution line.

Since the panels will be ground-mounted and the total nameplate capacity is over 12 kW, the Project is considered to be a Class 3 Solar Facility according to the classification presented in Ontario Regulation 521/10.

Table 2.1 General Project Description

Project Description	Ground-mounted Solar PV, Class 3
System Nameplate Capacity	10 MW AC
Local Distribution Company	N/A

2.1 Project Location

The Project Location¹ will be on privately owned land, zoned rural, totalling approximately 46 ha. Figure A.1 in Appendix A shows the zoning designation plan. Also, Figure A.2 presents the Project Area Location Plan.

2.2 Acoustical Environment

The Project will be surrounded by heavily forested areas to the west, east and south. The background noise levels are expected to be typical of rural areas, classified as a Class 3 based on Publication NPC-232 by the MOE. Major high voltage transmission lines pass within 0.5 km to the east of the site. The Trans-Canada Highway passes both to the south and to the west at a minimum distance of 6.5 km. The Town of Cochrane is situated approximately 19 km to the southeast. There are no airports within 5 km of the Project Location.

2.3 Life of Project

The expected life of the Project is 30 years. The manufacturer's warranty on the PV modules is 25 years and the expected life of solar power plants of this type is typically 35 to 40 years. At that time (or earlier if the 20-yr power purchase agreement is not extended), the Project will be decommissioned or refurbished depending on market conditions and/or technological changes.

2.4 Operating Hours

Solar PV facilities produce electricity during the day hours, when the sun rays are collected by the panels. After sunset the facility will not receive solar radiation to generate any electricity. Under these conditions the inverters will not produce any noise and the transformers will be energized, but not in operation (no fans in operation).

2.5 Approach to the Study

The sound pressure levels at the POR were predicted using procedures from ISO 9613-2, which is a widely used and generally accepted standard for the evaluation of noise impact in environmental Assessments. The sound power level for the inverters was provided by the manufacturer while the sound power level for the transformers was estimated. The software package CADNA-A, which implements ISO-9613-2, was used to predict the noise levels at the POR. This numerical modeling software is able to simulate sound sources as well as sound mitigation measures taking into account atmospheric and ground attenuation. Some of the CADNA-A configurations used in the modeling are shown in Figure 2.1.

¹ "Project Location" in the context of this study is an area occupied by the Project infrastructure.

Elevation contours were not included in the CADNA-A model. This conservative approach was applied in order to avoid including any barrier effects of ground surface obstacles.

For modeling purposes, the vegetation that blocks some of the POR from the sources has not been incorporated.

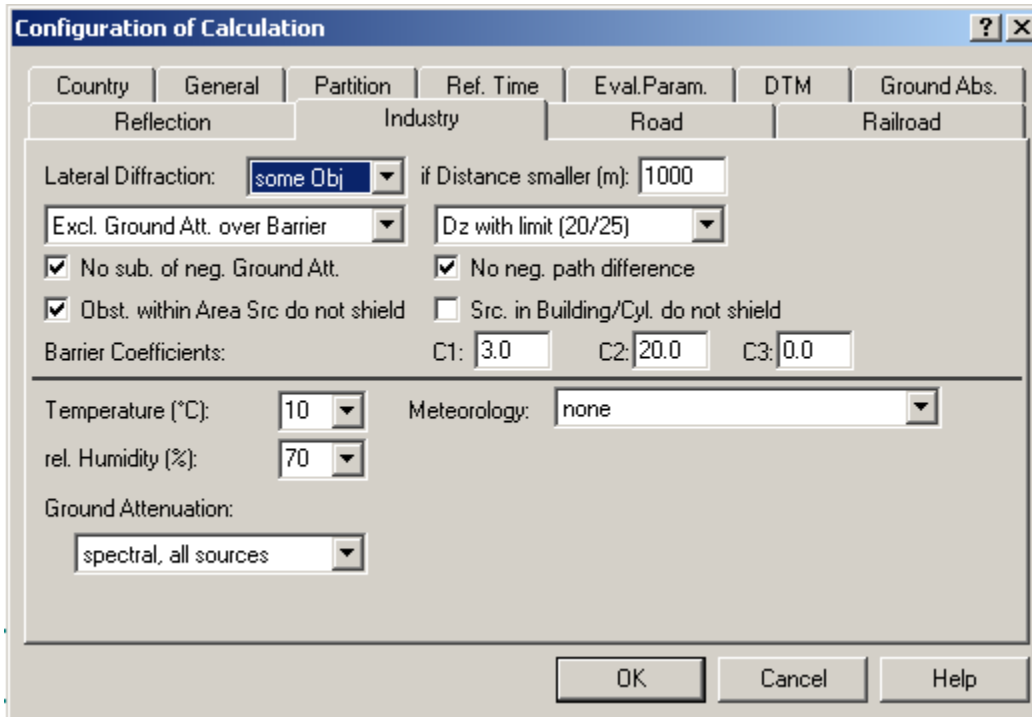


Figure 2.1 CADNA-A Configurations

3. Noise Sources

The main sources of noise from the Project will be seven inverter clusters, each one containing two inverters and one medium-voltage transformer, and a substation containing the main step-up transformer. The Project layout is provided in Figure A.2. The coordinates of each noise source are presented in Table B.1 of Appendix B.

All noise sources were modeled as non-directional point sources.

Switchgear and a small step-down transformer used for lighting, located at the substation, do not emit any significant noise and consequently have not been considered as sources of noise.

For the purpose of this study it is assumed that all inverters and transformers will be operating 24 hours at full capacity.

3.1 Substation Transformer

A 10-MVA step-up transformer that will step up the 27.6-kV power to 115 kV, required by the local distribution company, will be located in the substation. The transformer manufacturer provided an expected overall sound pressure level of 66 dB (measured in accordance with the IEEE C57.12.90-2010 standard). The transformer will be of ONAF (oil natural air forced) type and will look similar

to the one shown in Figure B.2. The sound power spectrum was determined using the provided overall sound pressure level (66 dB), a characteristic area of 100-m² over which the sound pressure acts (using 125% of the encompassing vertical surface area), and empirical correlations for transformer noise (Crocker, 2007). This calculation is available in Figure B.3 of Appendix B. Noise source height representing the transformer was assumed at 3.6 m above grade.

Power transformers are considered by the MOE to be tonal noise sources. A 5-dB penalty was added to the sound power spectrum, as recommended by Publication NPC-104, “Sound Level Adjustments” for tonality.

Table B.2 in Appendix B shows the frequency spectrum used to model the substation transformer.

3.2 Inverter Clusters

Northland is planning to use inverters manufactured by SMA. Seven inverter clusters will be installed as part of the Project. Each cluster comprises of two SMA Sunny Central 800CP inverters and one medium voltage transformer. A schematic layout with approximate dimensions of such cluster is available in Figure 3.1, additional information regarding details of the inverter cluster can be found in Appendix B). The cluster components listed above were modeled as point sources shown in Figure 3.2. Note that the planned enclosure over the inverters was not taken into account as a mitigation measure in the noise model.

The installed capacity of each Sunny Central 800CP inverter is 800 kW. SMA provided third-octave noise data for the Sunny Central 800CP inverter (Figure B.1 of Appendix B). The provided third octave spectrum was converted to a full octave spectrum and the contribution from two inverters was combined into a single sound power spectrum for use with CADNA-A model (calculations are available in Figure B.4 of Appendix B). A 5-dBA penalty was added to the frequency spectrum, as stipulated in Publication NPC-104, “Sound Level Adjustments,” to allow for tonality. The frequency spectrum used to model combined noise emission from the two inverters located next to each other within the same cluster is shown in Table B.2 of Appendix B.

A 1.6-MVA transformer used to step up the 360-V power from the inverters to 27.6 kV will be located in close proximity to the inverters. Since the transformer make and model have not been selected at this point (although it is known that the transformer will be of ONAN (oil natural air natural) type, the sound power levels resulting from the operation of the transformer were evaluated using data from NEMA TR 1-1993 (R2000) and a surface area of 36.8-m² over which the overall sound pressure acts (evaluated in accordance with IEEE C57.12.90-2010). The NEMA levels were then converted into frequency spectrum using empirical correlations for transformer noise (Crocker, 2007). This calculation is available in Figure B.5 of Appendix B. Power transformers are considered by the MOE to be tonal noise sources. A 5-dB penalty was added to the sound power spectrum, as recommended by Publication NPC-104, “Sound Level Adjustments” for tonality.

Table B.2 in Appendix B shows the frequency spectrum used to model the transformers located in the clusters.

Although for the modeling purposes it was assumed that the facility will operate 24 h at full capacity, in reality at night the facility will be idle. Under these conditions the inverters do not produce noise. The transformers (at the substation and clusters) are energized and make some magnetostrictive noise at a reduced level, but no cooling fans are in operation.

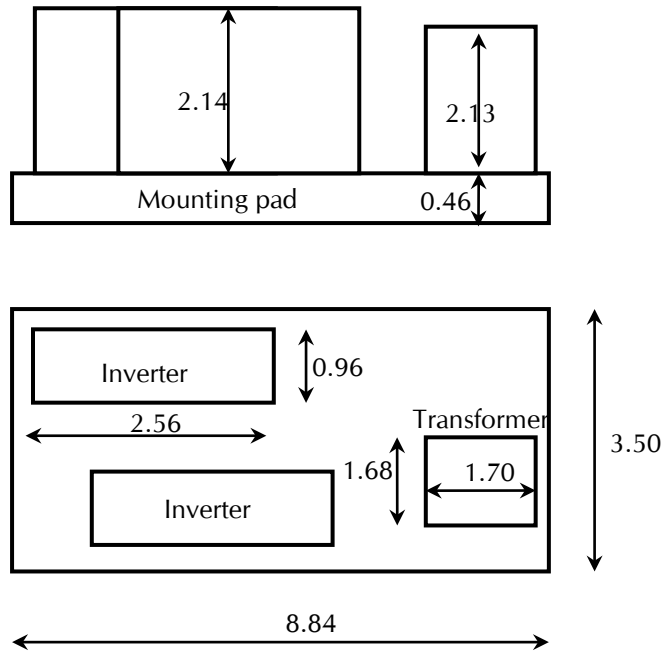


Figure 3.1 Schematic Inverter Cluster Layout
(all dimensions in metres)

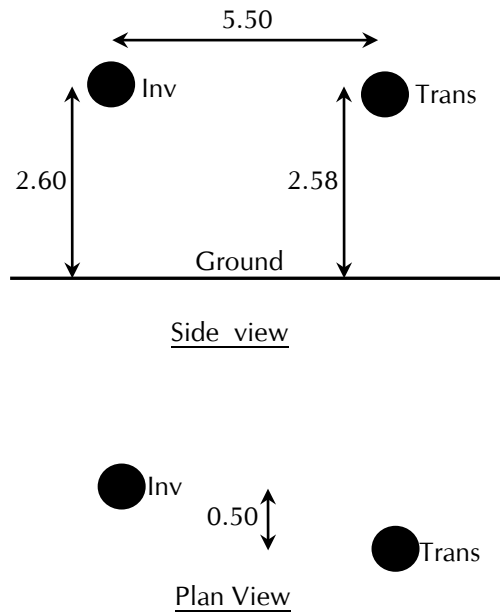


Figure 3.2 Inverter Cluster CADNA-A Acoustical Model

where: Inv = Noise Source Representing Two Sunny Central 800CP Inverters; and Trans = Noise Source Representing 360-V/27.6-kV/1.6-MVA Cluster Transformer (all dimensions in metres).

3.3 Noise Summary Table

A summary of the sound sources described above, including sound power level, characteristics and proposed noise control measures, is presented in Table 3.1.

Table 3.1 Noise Source Summary for Long Lake Solar Project

Source ID	Description	Total Sound Power Level (dBA)	Source Location	Sound Characteristics	Noise Control Measures
Sub	27.6-kV/115-kV/10-MVA substation transformer	93.4	O	S-T	U
Inv1	Two Sunny Central 800CP inverters at Cluster 1	91.3	O	S-T	U
Inv2	Two Sunny Central 800CP inverters at Cluster 2	91.3	O	S-T	U
Inv3	Two Sunny Central 800CP inverters at Cluster 3	91.3	O	S-T	U
Inv4	Two Sunny Central 800CP inverters at Cluster 4	91.3	O	S-T	U
Inv5	Two Sunny Central 800CP inverters at Cluster 5	91.3	O	S-T	U
Inv6	Two Sunny Central 800CP inverters at Cluster 6	91.3	O	S-T	U
Inv7	Two Sunny Central 800CP inverters at Cluster 7	91.3	O	S-T	U
Trans1	360-V/27.6-kV/1.6-MVA cluster transformer at Cluster 1	84.1	O	S-T	U
Trans2	360-V/27.6-kV/1.6-MVA cluster transformer at Cluster 2	84.1	O	S-T	U
Trans3	27.6-kV/1.6-MVA cluster transformer at Cluster 3	84.1	O	S-T	U
Trans4	360-V/27.6-kV/1.6-MVA cluster transformer at Cluster 4	84.1	O	S-T	U
Trans5	360-V/27.6-kV/1.6-MVA cluster transformer at Cluster 5	84.1	O	S-T	U
Trans6	360-V/27.6-kV/1.6-MVA cluster transformer at Cluster 6	84.1	O	S-T	U
Trans7	360-V/27.6-kV/1.6-MVA cluster transformer at Cluster 7	84.1	O	S-T	U

Notes:

1. A 5-dBA penalty is included in this table.
2. Location: Inside building (I), Outside building (O).
3. Sound Characteristics: Steady (S), Tonal (T), Impulsive (I), Quasi-Steady Impulsive (QSI).
4. Noise Control: Silencer (S), Acoustic lining (A), Barrier (B), Lagging (L), Enclosure (E), Other (O), Uncontrolled (U).

3.4 Adjacent Solar Projects

To identify the adjacent solar projects Hatch's internal database of solar projects and MOE records available in http://www.ene.gov.on.ca/environment/en/subject/renewable_energy/projects/index.htm were searched (August 13, 2012).

There are no Noise Receptors that are within 1 km of equipment in the Project and any adjacent project. As a result, there are no adjacent projects included in this study.

4. Noise Receptors and Points of Reception

The Noise Receptors used in this study were identified from the OBM and Google Earth Pro aerial imagery (July 2004) within 1 km distance from the Project Site² boundary, and also from visual observations of the Project Site surroundings conducted in Summer 2010.

The Noise Receptors corresponding to the vacant lots were added based on parcel information provided by First Base Solutions (Teranet Data) and located according to the requirements outlined in Ontario Regulation 359/09, and its amendment (Ontario Regulation 521/10).

The total number of Noise Receptors within a 1 km distance from the Long Lake Solar Project, Project Site boundary is 17, including the vacant lots. Points of reception (POR) representing the noise receptors were located at the center of house footprint (Noise Receptor center) elevated 4.5 m above ground. Also, noise compliance was verified within 30-m distance from the Noise Receptor centers at 1.5 m above the ground.

Three POR, identified in Table 4.1, were chosen as representative for evaluating the noise contribution from each individual source. These three POR were chosen in order to represent sound pressure level contributions on different areas around the Project Location. The complete set of results for all considered POR is provided in Table 6.2.

² "Project Site" in the context of this study is the complete area designated for the Project but not necessarily occupied with the project infrastructure. Project Location is always contained within Project Site.

Table 4.1 Point of Reception at 4.5 m Noise Impact from Individual Noise Sources of Long Lake Solar Project

Source ID	Noise Receptor ID					
	7		8		9	
	Distance (m)	Leq Sound Level (dBA)	Distance (m)	Leq Sound Level (dBA)	Distance (m)	Leq Sound Level (dBA)
Sub	889.5	21.9	285.6	32.8	277.6	33.1
Inv1	864.5	19.6	205.5	33.0	425.9	26.6
Inv2	969.7	18.4	358.3	28.2	624.3	22.9
Inv3	717.4	21.5	239.3	31.7	552.0	24.1
Inv4	867.6	19.6	434.3	26.4	747.1	21.1
Inv5	691.4	21.9	498.3	25.1	790.0	20.5
Inv6	512.4	24.8	373.5	27.8	627.0	22.9
Inv7	358.2	28.2	334.7	28.8	493.5	25.2
Trans1	859.8	12.6	201.2	26.4	425.2	19.7
Trans2	965.6	11.4	356.2	21.3	624.0	15.9
Trans3	713.7	14.6	241.7	24.8	554.1	17.1
Trans4	864.7	12.6	435.9	19.4	748.8	14.1
Trans5	694.1	14.8	495.0	18.2	787.5	13.5
Trans6	515.8	17.8	368.9	21.0	623.8	15.9
Trans7	362.8	21.1	329.2	22.0	489.2	18.3

5. Mitigation Measures

The analysis indicates that no mitigation measures are necessary to meet the MOE requirement of 40 dBA for all POR.

6. Impact Assessment

The purpose of the acoustic Assessment report is to demonstrate that the facility is in compliance with the noise performance limits. The Project will be located in a Class 3 Area, based on the classification defined in Publication NPC-232 by the MOE. Class 3 area means a rural area with an acoustical environment that is dominated by natural sounds, with little or no traffic noise, such as an agricultural area.

Table 6.1 shows the performance limits set by the MOE for Class 3 Areas, according to Publication NPC-232.

Table 6.1 Performance Limits (One-Hour L_{eq}) by Time of Day for Class 3 Areas

Time of Day	One Hour L_{eq} (dBA) Class 3 Area
07:00 to 19:00	45.0
19:00 to 23:00	40.0
23:00 to 07:00	40.0

The solar facility will be operating during the daylight hours, that is, between 07:00 and 19:00 during most days of the year. However, in the summer months the sun may shine before 07:00 or until past 19:00. As such, during the summer the facility will be operating at the time when the applicable performance limit changes from 45 dBA to 40 dBA. Also, the transformers remain energized at night. In order to account for this, the study assumes that the facility will be operating 24 hours and compares the impact from the facility with the 40-dBA limit. In reality, the cooling fans will not be in operation at night.

For this study, the overall ground attenuation coefficient was estimated to be 0.7. Appendix D includes a list of all the parameters used in the CADNA-A model to predict the sound pressure levels at the POR.

The modelling does not consider the effect of the solar panels on the predicted sound pressure levels at the points of reception. The solar panels may act as barriers to further reduce noise at the POR.

6.1 Compliance with Performance Limits

Table 6.2 presents the predicted sound pressure levels for the POR located within 1 km from the Project Site. Sound pressure contours at 4.5-m and 1.5-m are available in Figure C.1 and Figure C.2. Appendix D includes a detailed calculation log of the representative POR with the highest sound pressure level.

Effect of the noise emissions at the Noise Receptors was also assessed by intersecting the 40-dBA sound pressure contours calculated at 1.5-m above ground with 30-m radius circles placed around the Noise Receptor centers (Figure C.2). The results show that none of the 30-m radius zones are affected by the noise emissions.

Table 6.2 Calculated Sound Pressure Levels at POR within 1 km of Long Lake Solar Project
(Shaded rows correspond to representative POR)
Existing = Existing dwelling, Vacant = Vacant Lot.
The performance limit is 40.0-dBA.

Noise Receptor ID	Description	Sound Pressure Level (dBA)	Performance Limit (dBA)	POR Height (m)	Min distance to Source (m)	POR UTM Coordinates NAD 83 Zone 17 (m)	
						X	Y
1	Vacant	23.8	40.0	4.5	1203	477811.8	5443763.9
2	Vacant	25.6	40.0	4.5	1008	477980.0	5443593.6
3	Existing	28.8	40.0	4.5	679	478319.8	5443635.5
4	Existing	28.3	40.0	4.5	704	478324.8	5443739.5
5	Existing	28.3	40.0	4.5	697	478339.8	5443757.5
6	Vacant	30.1	40.0	4.5	566	478433.2	5443623.4
7	Vacant	32.9	40.0	4.5	358	478709.6	5443720.3
8	Existing	39.8	40.0	4.5	201	479315.6	5443455.5
9	Vacant	36.1	40.0	4.5	278	479395.3	5443758.5
10	Vacant	34.4	40.0	4.5	304	479825.0	5443738.7
11	Vacant	30.4	40.0	4.5	532	480081.5	5443740.3
12	Existing	27.0	40.0	4.5	872	480085.8	5442506.5
13	Existing	23.4	40.0	4.5	1207	480110.8	5444640.5
14	Existing	23.7	40.0	4.5	1267	480156.7	5442064.9
15	Existing	23.0	40.0	4.5	1245	480205.8	5444632.5
16	Existing	25.7	40.0	4.5	1006	480222.5	5442454.5
17	Existing	22.9	40.0	4.5	1361	480419.8	5442149.5

The results of this study show that all POR are compliant with MOE guidelines based on the performance limit of 40 dBA.

7. Conclusions and Recommendations

For the Long Lake Solar Project, the sound pressure levels at the POR have been estimated using the CADNA-A model, based on ISO 9613-2. No mitigations are required for the Project operation.

Based on the results obtained in this study, it is concluded that the sound pressure levels at the POR, resulting from the Long Lake Solar Project operation, will be below MOE requirements for Class 3 areas of 40 dBA at all times.

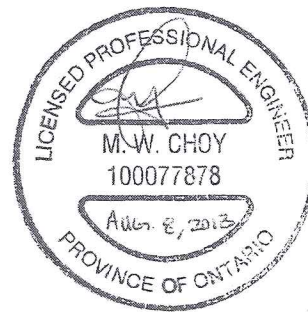
8. Signatures

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Appendix A

Land Use Zoning Designation Plan and Area Location Plan

Figure A.1 Land Use Zoning Designation Plan

Insert in original size and orientation

Figure A.2 Area Location Plan

Insert in original size and orientation.

Appendix B

Noise Sources

Table B.1 Point Sources from Long Lake Solar Project Used in CADNA-A, Includes Tonality Penalty of 5.0-dBA

Source ID	Description	Spectra ID	Total sound power level (dBA)	Correction (dBA)	Height (m)	Coordinates, UTM NAD 83 Zone 17 (m)		
						X	Y	Z
Sub	27.6-kV/115-kV/10-MVA substation transformer	T115kV_10MVA	93.4	5.0	3.60	479583.5	5443554.4	3.60
Inv1	Two Sunny Central 800CP inverters at Cluster 1	SMA_SC800CPX2	91.3	5.0	2.60	479487.2	5443342.6	2.60
Inv2	Two Sunny Central 800CP inverters at Cluster 2	SMA_SC800CPX2	91.3	5.0	2.60	479487.2	5443141.0	2.60
Inv3	Two Sunny Central 800CP inverters at Cluster 3	SMA_SC800CPX2	91.3	5.0	2.60	479233.8	5443230.6	2.60
Inv4	Two Sunny Central 800CP inverters at Cluster 4	SMA_SC800CPX2	91.3	5.0	2.60	479233.8	5443029.0	2.60
Inv5	Two Sunny Central 800CP inverters at Cluster 5	SMA_SC800CPX2	91.3	5.0	2.60	478982.5	5443085.0	2.60
Inv6	Two Sunny Central 800CP inverters at Cluster 6	SMA_SC800CPX2	91.3	5.0	2.60	478982.5	5443286.6	2.60
Inv7	Two Sunny Central 800CP inverters at Cluster 7	SMA_SC800CPX2	91.3	5.0	2.60	478982.5	5443488.2	2.60
Trans1	360-V/27.6-kV/1.6-MVA cluster transformer at Cluster 1	T27.6kV_1.6MVA	84.1	5.0	2.58	479481.7	5443342.1	2.58
Trans2	360-V/27.6-kV/1.6-MVA cluster transformer at Cluster 2	T27.6kV_1.6MVA	84.1	5.0	2.58	479481.7	5443140.5	2.58
Trans3	360-V/27.6-kV/1.6-MVA cluster transformer at Cluster 3	T27.6kV_1.6MVA	84.1	5.0	2.58	479228.3	5443230.1	2.58
Trans4	360-V/27.6-kV/1.6-MVA cluster transformer at Cluster 4	T27.6kV_1.6MVA	84.1	5.0	2.58	479228.3	5443028.5	2.58
Trans5	360-V/27.6-kV/1.6-MVA cluster transformer at Cluster 5	T27.6kV_1.6MVA	84.1	5.0	2.58	478988.0	5443084.5	2.58
Trans6	360-V/27.6-kV/1.6-MVA cluster transformer at Cluster 6	T27.6kV_1.6MVA	84.1	5.0	2.58	478988.0	5443286.1	2.58
Trans7	360-V/27.6-kV/1.6-MVA cluster transformer at Cluster 7	T27.6kV_1.6MVA	84.1	5.0	2.58	478988.0	5443487.7	2.58

Table B.2 Frequency Spectra Used for Modelling the Noise Sources, Not Including Tonality Penalty

Spectra ID	Octave Spectrum (dBA)										
	31.5	63	125	250	500	1000	2000	4000	8000	A	lin
SMA_SC800CPX2		63.1	73.9	80.5	82.3	78.7	74.1	65.0	72.7	86.3	95.0
T27.6kV_1.6MVA	36.3	55.5	67.6	70.1	75.5	72.7	68.9	63.7	54.6	79.1	87.7
T115kV_10MVA	45.6	64.8	76.9	79.4	84.8	82	78.2	73	63.9	88.4	97

Insert 4 pages: Appendix B - Inverter Specs - SMA SUNNY CENTRAL 720CP-760CP-800CP.pdf

Terz-midle-frequency [kHz]	Soundpower-level L_{xpA} [dB _A]500kW	Soundpower-level L_{xpA} [dB _A]640kW	Soundpower-level L_{xpA} [dB _A]720kW	Soundpower-level L_{xpA} [dB _A]760kW	Soundpower-level L_{xpA} [dB _A]800kW
0,05	63,30	55,30	57,70	67,00	56,50
0,063	60,80	53,10	56,80	63,20	54,00
0,08	63,90	56,30	56,50	59,50	55,20
0,1	64,10	66,20	65,00	66,50	68,10
0,125	65,70	64,50	60,60	65,20	62,00
0,16	72,30	65,80	65,50	63,20	66,40
0,2	67,30	64,60	66,80	64,90	67,80
0,25	66,10	76,20	77,50	70,80	72,40
0,315	78,40	79,80	77,70	82,20	75,10
0,4	73,70	73,90	73,90	72,80	66,70
0,5	77,80	78,70	77,70	77,40	74,70
0,63	78,90	78,90	74,60	77,40	77,00
0,8	70,60	72,50	74,10	70,60	72,00
1	72,20	71,00	70,00	68,90	67,90
1,25	72,40	72,00	71,50	70,80	71,80
1,6	67,30	68,30	76,70	68,60	68,50
2	69,30	66,30	66,50	67,20	65,30
2,5	65,10	66,80	64,60	64,80	63,90
3,15	62,60	64,30	65,00	63,20	61,00
4,0	53,50	54,20	54,70	52,30	53,80
5,0	51,30	49,50	50,50	51,20	49,80
6,3	68,90	72,60	73,50	73,50	69,70

SC800CP at nominal power of 800 kW at 60 Hz

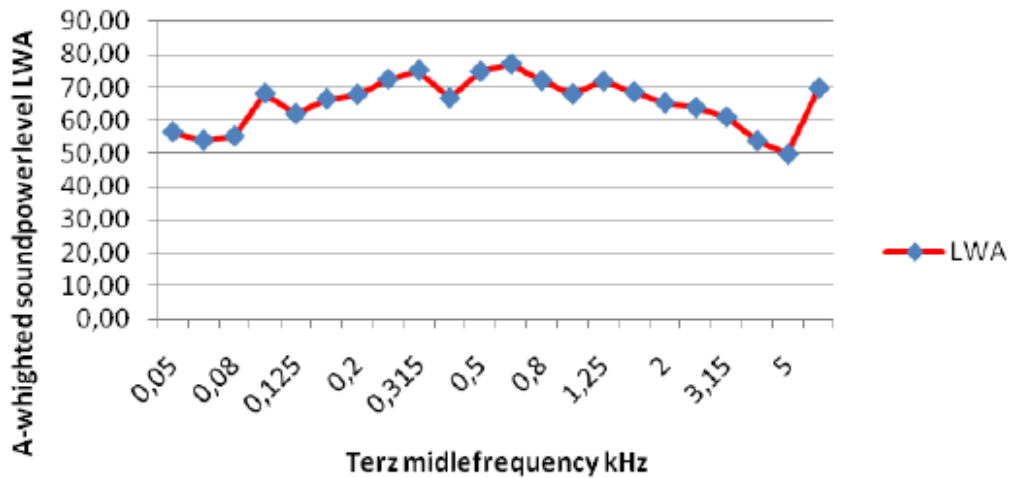


Figure B.1 SC800CP Inverter Sound Power Level as Provided by SMA. Note that the Header in the Table above Represents Various Inverter Models of CS###CP Series.

Insert: Figure B.2 – Similar Transformer Dimensions

Estimated Frequency Spectra for Transformers

Transformer - 115kV/10MVA

From Handbook of Noise and Vibration Control (Crocker, 2007, page 1335-1336, Eq. 18 and Table 20)

Average Lp 66 dB Guaranteed sound pressure level provided by transformer manufacturer
 Estimated surface area 100.0 m² Estimated based on similar transformer dimensions and IEEE C57.90-2010 standard

Correction factors are in dB

Freq. (Hz)	31	63	125	250	500	1000	2000	4000	8000	Notes
C1	-11.0	-5.0	-3.0	-8.0	-8.0	-14.0	-19.0	-24.0	-31.0	Outdoors, indoors in mechanical room over 140 m ³ Indoors Serious Noise Problems
C2	-11	-2	3	-2	-2	-11	-19	-24	-31	
C3	-11	-2	3	2	2	-4	-9	-14	-21	

Sound Power Level calculated as $L_w = \text{Average } L_pA + 10 \cdot \log(\text{Estimated surface area}) + C + 10$

Freq. (Hz)	31	63	125	250	500	1000	2000	4000	8000	Combined [dB]
C1 based [dB]	85.0	91.0	93.0	88.0	88.0	82.0	77.0	72.0	65.0	97.0
C2 based [dB]	85.0	94.0	99.0	94.0	94.0	85.0	77.0	72.0	65.0	102.1
C3 based [dB]	85.0	94.0	99.0	98.0	98.0	92.0	87.0	82.0	75.0	104.1

Resulting A-weighted sound power level

Freq. (Hz)	A-Weight	C1 based [dBA]	C2 based [dBA]	C2 based [dBA]
31	-39.4	45.6	54.6	59.6
63	-26.2	64.8	67.8	67.8
125	-16.1	76.9	82.9	82.9
250	-8.6	79.4	85.4	89.4
500	-3.2	84.8	90.8	94.8
1000	0	82.0	85.0	92.0
2000	1.2	78.2	78.2	88.2
4000	1	73.0	73.0	83.0
8000	-1.1	63.9	63.9	73.9
LwA [dBA]		88.4	93.3	98.2

 Used in the study

Figure B.3 Sound Power Level Calculation for 27.6-kV/115-kV/10-MVA Substation Transformer.

Sound Power Level Calculation for SMA Sunny Central 800CP, 100% LOAD

Third octave, as provided		
Freq #	Freq (Hz)	LwA (dBA)
1	25	
2	31.5	
3	40	
4	50	56.5
5	63	54.0
6	80	55.2
7	100	68.1
8	125	62.0
9	160	66.4
10	200	67.8
11	250	72.4
12	315	75.1
13	400	66.7
14	500	74.7
15	630	77.0
16	800	72.0
17	1000	67.9
18	1250	71.8
19	1600	68.5
20	2000	65.3
21	2500	63.9
22	3150	61.0
23	4000	53.8
24	5000	49.8
25	6300	69.7
26	8000	
27	10000	
Total LwA		83.3

Full octave, as used in CADNA-A model			
Freq #	Freq (Hz)	LwA 1 inverter (dBA)	LwA 2 inverters (dBA)
	31.5		
5	63	60.1	63.1
8	125	70.9	73.9
11	250	77.5	80.5
14	500	79.3	82.3
17	1000	75.7	78.7
20	2000	71.1	74.1
23	4000	62.0	65.0
26	8000	69.7	72.7
Total LwA		83.3	86.3

$$10 \log \left(10^{\frac{56.5}{10}} + 10^{\frac{54.0}{10}} + 10^{\frac{55.2}{10}} \right) = 60.1 \text{ dBA}$$

$$10 \log \left(10^{\frac{60.1}{10}} + 10^{\frac{60.1}{10}} \right) = 63.1 \text{ dBA}$$

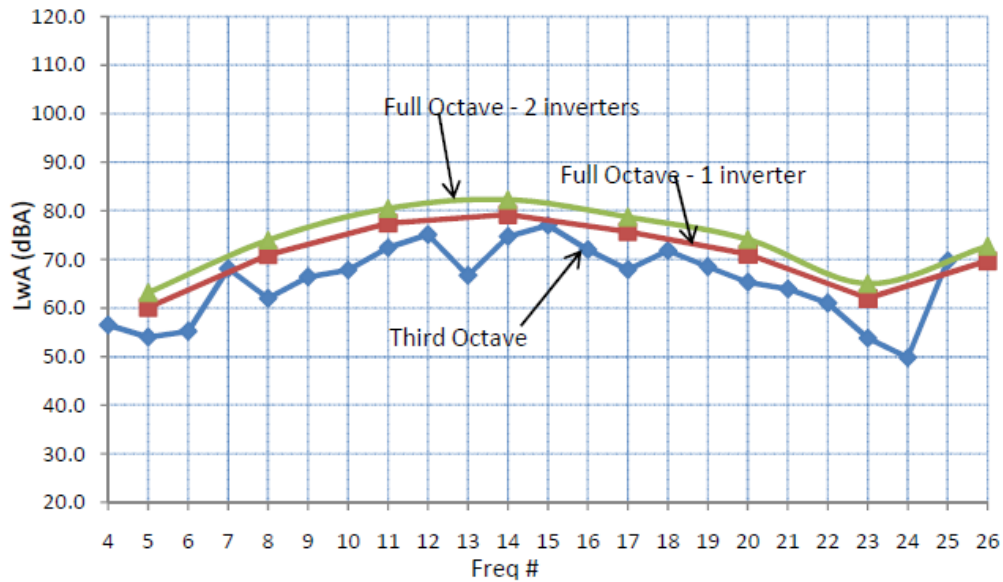


Figure B.4 Sound Power Level Calculation for SMA Sunny Central 800CP, 100% LOAD.

Estimated Frequency Spectra for Transformers

Transformer - 27.6kV/1.6MVA

From Handbook of Noise and Vibration Control (Crocker, 2007, page 1335-1336, Eq. 18 and Table 20)

Average Lp 61 dB Based on NEMA TR1-1993 (R2000), Table 0-2
 Estimated surface area 36.8 m² Estimated based on similar transformer dimensions and IEEE C57.90-2010 standard

Correction factors are in dB

Freq. (Hz)	31	63	125	250	500	1000	2000	4000	8000	Notes
C1	-11.0	-5.0	-3.0	-8.0	-8.0	-14.0	-19.0	-24.0	-31.0	Outdoors, indoors in mechanical room over 140 m ³
C2	-11	-2	3	-2	-2	-11	-19	-24	-31	Indoors
C3	-11	-2	3	2	2	-4	-9	-14	-21	Serious Noise Problems

Sound Power Level calculated as $L_w = \text{Average LpA} + 10 \cdot \log(\text{Estimated surface area}) + C + 10$

Freq. (Hz)	31	63	125	250	500	1000	2000	4000	8000	Combined [dB]
C1 based [dB]	75.7	81.7	83.7	78.7	78.7	72.7	67.7	62.7	55.7	87.7
C2 based [dB]	75.7	84.7	89.7	84.7	84.7	75.7	67.7	62.7	55.7	92.7
C3 based [dB]	75.7	84.7	89.7	88.7	88.7	82.7	77.7	72.7	65.7	94.8

Resulting A-weighted sound power level

Freq. (Hz)	A-Weight	C1 based [dBA]	C2 based [dBA]	C2 based [dBA]
31	-39.4	36.3	45.3	50.3
63	-26.2	55.5	58.5	58.5
125	-16.1	67.6	73.6	73.6
250	-8.6	70.1	76.1	80.1
500	-3.2	75.5	81.5	85.5
1000	0	72.7	75.7	82.7
2000	1.2	68.9	68.9	78.9
4000	1	63.7	63.7	73.7
8000	-1.1	54.6	54.6	64.6
LwA [dBA]		79.0	84.0	88.8

 Used in the study

Figure B.5 Sound Power Level Calculation for 360-V/27.6-kV/1.6-MVA Cluster Transformer.

Appendix C

Noise Maps from CADNA-A

Figure C.1 Noise Map at 4.5-m.
Insert in original size and orientation.

Figure C.2 Noise Map at 1.5-m.
Insert in original size and orientation.

Appendix D

CADNA-A Sample Calculations

Insert: Appendix D - CADNA-A sample calculations.pdf